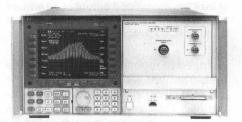


SERVICE INFORMATION FROM HEWLETT-PACKARD

1st Quarter 1994

The Optical Spectrum Analyzer - Part 3 Sensitivity

Mike Levernier/Hewlett-Packard



Introduction

In the previous issue of Bench Briefs Richard Ogg explained the optical spectrum analyzer in terms of signal processing, various operating modes, noise generation, and the control of noise through filtering schemes. In this issue, Mike Levernier describes OSA sensitivity through Hewlett-Packard's patented way of allowing the user to directly enter the required sensitivity level - what HP calls a "sensitivity function." For more detailed information on optical spectrum analysis basics, order Application Note 1550-4, Optical Spectrum Analysis, HP Pub. No. 5091-3054E from your local HP sales/service office.

Sensitivity – Directly Settable by the User

Sensitivity is defined as the minimum detectable signal or, more specifically, six times the rms noise level of the instrument. Sensitivity is not specified as the average noise level, as it is for RF and microwave spectrum analyzers, because the average noise level of optical spectrum analyzers is 0 watts (or minues infinity dBm). (For more information on the differences between electrical and optical spectrum analyzers, see the previous issue of *Bench Briefs*.) Figure 1 shows the display of a signal that has an amplitude equal to the sensitivity setting of the optical spectrum analyzer.

Single monochromators typically have sensitivity about 10 to 15 dB better than that of double monochromators due to the additional loss of the second diffraction grating in double monochromators. The double-pass monochromator has the same high sensitivity of single monochromators even though the light strikes the diffraction grating twice. The high sensitivity is made possible by the halfwave plate and the use of a smaller photodetector that has a lower noise equivalent power (NEP).

Sensitivity can be set directly on Hewlett-Packard optical spectrum analyzers, which then automatically adjust to optimize the sweep time, while maintaining the desired sensitivity. Sensitivity is coupled directly to video bandwidth, as shown in Figure 2. As the sensitivity level is lowered, the video bandwidth is decreased (or the transimpedance amplifier gain is increased), which results in a longer sweep time, since the sweep time is inversely proportional to the video bandwidth. The sweep time can be optimized because the video bandwidth is continuously variable and just enough video filtering can be performed. This avoids the problem of small increases in sensitivity causing large increases in sweep time, which can occur when only a few video bandwidths are available in fairly large steps.

Tuning Speed

Sweep-Time Limits

For fast sweeps, sweep time is limited by the maximum tuning rate of the monochromator. The direct-drive-

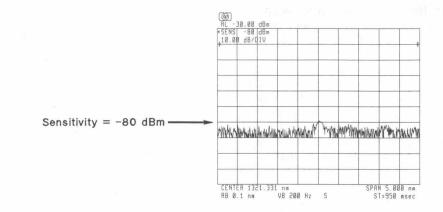


Figure 1. Display of signal with amplitude equal to sensitivity level.

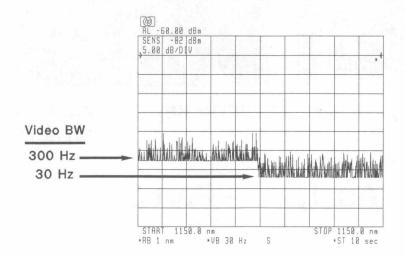


Figure 2. Video bandwidth directly affects sensitivity.

motor system allows faster sweep rates when compared with optical spectrum analyzers that use gear-reduction systems to rotate the diffraction grating.

For high-sensitivity sweeps that tend to be slower, the small photodetector and continuously variable digital video bandwidths allow faster sweep times. The small photodetector reduces the sweep time because it has a lower NEP than the large photodetectors used in other optical spectrum analyzers. Lower NEP means that for a given sensitivity level, a wider video bandwidth can be used, which results in a faster sweep. (Sweep time is inversely proportional to the video bandwidth for a given span and resolution bandwidth.)

The continuously variable digital video bandwidths improve the sweep time for high-sensitivity sweeps in two ways. First, the implementation of digital video filtering is faster than the response time required by narrow analog filters during autoranging. Second, since the video bandwidth can be selected with great resolution, just enough video filtering can be used, resulting in no unnecessary sweep-time penalty due to using a narrower video bandwidth than is required. Figure 3 shows a 20 second filter-response measurement. This filter, for an erbium amplifier, was stimulated by a white-light source and the figure shows the normalized response. The purpose of this filter is to attenuate light at the pump wavelength, while passing the amplified laser output of 1550 nm. Due to the low power level of white-light sources, this measurement requires great sensitivity, which traditionally has resulted in long sweep times.

Autoranging Mode

Autoranging mode is activated automatically for sweeps with amplitude ranges greater than about 50 dB. The amplitude range is determined by the top of the screen and the sensitivity level set by the user. With the autoranging mode activated, when the signal amplitude crosses a threshold level, the sweep pauses, the transimpedance amplifier's gain is

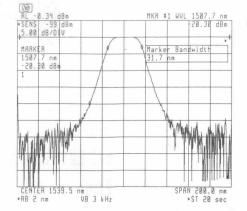


Figure 3. Improved sweep times, even for high sensitivity measurements that traditionally result in slow sweeps. This plot shows the normalized output of an erbium amplifier filter that was stimulated by a white-light source.

changed to reposition the signal in the measurement range of the analyzer's internal circuitry, and the sweep continues. This repositioning explains the pause that can occasionally be seen in a sweep with a wide measurement range.

Chopper Mode

The main purpose of the chopper mode is to provide stable sensitivity levels for long sweep times, which could otherwise be affected by drift of the electronic circuitry. The desired stability is achieved by automatically chopping the light to stabilize electronic drift in sweeps of 40 seconds or greater. The effect is to sample the noise and stray light before each trace point and subtract them from the

(See "Optical Spectrum Analyzer," page 8)

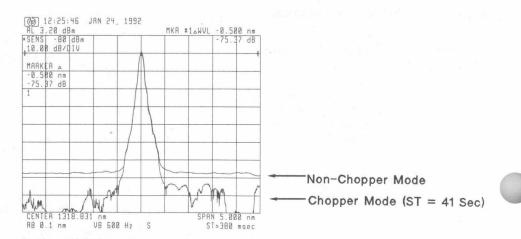
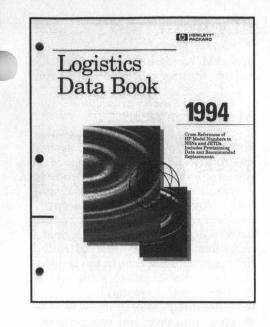


Figure 4. Dynamic range improvement from chopper mode.



1994 Logistics Data Book

John Cloutier/Hewlett-Packard

If your work requires U.S. Government National Stock Numbers (NSNs) for HP products and their components, HP's annual Logistic Data Book and its companion microfiche are must-have resources.

The data book cross references HP product numbers to National Stock Numbers (NSNs) and Joint Electronic Type Designators (JETDs), lists contract numbers for provisioned products, and recommends replacements for discontinued products. The companion microfiche lists NSNs for product components and can be requested with postage-paid cards included in the data books.

To obtain a free copy of the 1994 Logistics Data Book, contact your nearest HP office, or:

John Cloutier Hewlett-Packard Company Federal Support Services MS 51U-TH P.O. Box 58059 Santa Clara, CA 95052-8059

Safety-Related Service Notes

Service Notes from Hewlett-Packard relating to personal safety and possible equipment damage are of vital importance to our customers. To make you more aware of these important notes, they are printed on paper with a red border, and the service note number as an "-S" suffix. In order to make you immediately aware of any potential safety problems, we are highlighting safety-related service notes here with a brief description of each problem. Also, in order to draw your attention to safety-related service notes in the service note index, each safety-related service note is highlighted with a contrasting color.

HP E1401A VXI C-Size High-Power Mainframe Serial Numbers Affected 3227A00165 / 3227A00207

Build-up of surface contamination inside the E1401A power supply plus a jumper wire with damaged insulation may cause a shock hazard to exist on an externally-accessible pin on the rear panel of the E1401A.

Check your unit as follows: Connect a voltmeter between chassis ground and pin #23 on the Sub-D connector on the rear of the E1401A Mainframe. If a hazardous AC Voltage is present (greater than 30 VAC RMS, or 42 VAC peak), your unit is hazardous.

A new power supply must be installed. Order Safety Service Note E1401A-02-S (document ID number 5758 on the HP FIRST system) for more information.

E3910A/B PT500 Protocol Tester Serial Numbers Affected 08-0000 / CA33350292

E3939A/B PT500 Protocol Tester Serial Numbers Affected CA32220000 / CA33300023

E4093A/B PT500 Protocol Tester Serial Numbers Affected 02-0000 / CA33320025

E4095A/B PT500 Protocol Tester Serial Numbers Affected 03-0000 / CA33330209

E4100B PT500 Protocol Tester Serial Numbers Affected CA33130001 / CA33150006

IDAC-M-XPE PT500 Protocol Tester Serial Numbers Affected CA32090001 / CA33010010

IDAC-MPT PT500 Protocol Tester Serial Numbers Affected 01-0000 / 01-9999



High voltage applied to the connector module plane or connector module handle could cause the existing ground path to open, resulting in a possible shock hazard to the user.

Affected units must be retrofitted with grounding wires to rectify the problem. Contact your local HP sales/ service office and your unit will be repaired free of charge.

For more information, order the following Product Safety Service Notes using the HP FIRST FAX system.

Product Safety	HP FIRST
Service Note	Doc. ID No.
E3910A/B-02-S	5961
E3939A/B-02-S	5962
E4093A/B-02-S	5063
E4095A/B-02-S	5064
E4100B-02-S	5065
IDAC-M-XPE-02-S	5066
IDAC-MPT-02-S	5067

How is the Recommended Calibration Cycle Determined?

Jim Stead/Hewlett-Packard

Introduction

For T&M products, HP usually indicates in the manual a recommended calibration cycle. For many microwave instruments this is typically a one-year recommendation. With calibration costs rapidly increasing, longer calibration cycles are required to maintain a reasonable cost of ownership. Following is an explanation of some of the steps involved in determining how an extended cycle can be justified.

Past Experiences

Most companies maintain a database on past calibrations and can easily determine what percentage of instruments required adjustments. This data is then used to appropriately change the calibration cycle. HP maintains such a database for instruments used in our microwave instrument production facility. As an example, when the HP 8360 was introduced we looked at the data for a similar product, the HP 8340A. The data indicated that under normal operating conditions the recommended one-year calibration cycle for the HP 8340A was conservative (i.e.,

90% did not require any adjustments).

New Circuit Designs

Design improvements are also used to justify extended calibration cycles. Reduced parts count and fewer hardware adjustments mean there is less chance for drift or aging to have an effect on the calibration. In addition, newer circuit designs may provide better stability. When compared to the HP 8340A, the HP 8360 series has about one-third fewer components and about 25% of the HP 8340A hardware adjustments. Long-term ALC stability was also improved through the use of a Planar-Doped-Barrier (PDB) diode as the leveling detector.

User vs. Self Adjustments

Periodic adjustments are sometimes required for optimum performance. To maintain an extended calibration cycle, it is important that these adjustments are either done automatically by the instrument, or set up as user adjustments. Both the HP 8340A/B and HP 8360 series use auto tracking to maintain maximum RF output power. In addition, the HP 8360 series has both frequency span calibration and AM bandwidth calibration that fall into the user calibration category.

Mechanical Wear

Sometimes the instrument or system environment has a large influence on the long-term stability of the product. A good example is the HP 8510 system. Normal usage of a network analyzer requires that devices be connected and disconnected to make measurements. Over an extended time period this results in the connectors being subjected to wear and/or damage. For this reason, the HP 8510 recommended calibration cycle is limited to one year and will probably never be extended.

Conclusions

The recommended calibration cycle is just that; a recommendation. Operating environment and the user's application are variables that cannot be included in the manufacturer's recommendation. The published cycle should be used by the customer to help determine an initial calibration cycle. Then an ongoing data collection process should be initiated to determine the best calibration cycle for the customer's application.

1994 Bench Briefs' Instrument Service Note Index

HP FIRST (208)344-4809 T & M Section - Press 4 Password Section - Press 3 Password - 76683

SN Гуре	SN No.	in vi	Abstract Docum	HP FIRST nent ID No.
	3			E Arthur
MA	3324A-03		New firmware must be installed with new A6 Signal Source Board	5708
0	3456A-25		Clarification of product specifications and calibration cycle	5706
ИR	3457A-17		Modification prevents shorting of multiple channels	5985
0	35658-07		Reprogramming required for use with HP 35630A/B VISTA software	5977
0	3577A-17		Source harmonic distn spec changed from -30 dBc to -25 dBc	5978
0	3577B-07		Source harmonic distn spec changed from -30 dBc to -25 dBc	5979

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SN Type	SN No.	Abstract HP I Document I	FIRST D No.
MR	3589A-03	C1405A/B keyboard incompatibility with HP 3589A	5937
IO	3784A-03	Mod optimizes the HP 3784A for burst mode operation	5692
IO	3784A-04	Instructions to retrofit Opt 002 to a standard instrument	5693
MA	3784A-05	Mod to housing for pwr supply caps C1 and C2	5694
MA	3785A-25	Mod ensures conformance to performance test	5695
MR	4155A-01	Updating the preliminary ROMs with formal-released ROMs	5994
MR	4156A-01	Updating the preliminary ROMs with formal-released ROMs	5995
MR	4291A-01	New A3A3 assembly improves osc level (self-test 15)	5968
IO	4396A-08	New key cap for power line switch	5917
MR	4396A-09	New A3A3 assembly improves RF output level (self-test 16)	5969
MR	4396A-10	Modification prevents rubber key from sticking	5970
MR	4396A-11	Mod corrects PHASE LOCKED LOOP UNLOCKED error at high temp	5996
ΙΟ	4396A-12	Option upgrade procedures	5997
MA	4957A-01C	Available option allows high speed option retrofitting	5014
MR	4980A-11	LED board mod allows greater range of brightness adjustment	5929
MR	4981A-11	LED board mod allows greater range of brightness adjustment	5930
MR	4982A-11	LED board mod allows greater range of brightness adjustment	5931
IO	5071A-01	Unusual power-up seq can cause pseudo "Fatal Error" message	5719
IO	5071A-02	HP 5071A performance test	5720
IO	5529A-01A	List of software revision A.01.13 anomalies	5900
IO	5529V-01A	List of software revision A.01.13 anomalies	5901
MR	6060B-02	Safety compliance of RFI filter cap discharge time constant	5761
MR	6063B-02	Safety compliance of RFI filter cap discharge time constant	5762
IO	6651A-03	Mod reduces radiated RFI when replacing A2 HPIB board	5944
			5945
IO	6652A-03	Mod reduces radiated RFI when replacing A2 HPIB board Mod reduces radiated RFI when replacing A2 HPIB board	5945
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IO	6654A-03	Mod reduces radiated RFI when replacing A2 HPIB board	5948
IO	6655A-03	Mod reduces radiated RFI when replacing A2 HPIB board	5940 5949
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ΙΟ	8560A-27	Incorrect manual procedure cannot measure resol B/W accuracy	5714
MA	8560A-28	Diodes w/higher breakdown voltage improves focus reliability	5950
MR	8560E-02C	Recommended replacement of 5-volt regulators	5740
MA	8560E-06	Diodes w/higher breakdown voltage improves focus reliability	5951
MR	8560E-07	5-volt regulator reliability improvement on A6 pc board	5923
MR	8561B-25C	Recommended replacement of 5-volt regulators	5741
IO	8561B-27	Incorrect manual procedure cannot measure resol B/W accuracy	5715
MR	8561E-01C	Recommended replacement of 5-volt regulators	5742
MA	8561E-05	Diodes w/higher breakdown voltage improves focus reliability	5952
MR	8561E-06	5-volt regulator reliability improvement on A6 pc board	5924
MR	8562A-67C	Recommended replacement of 5-volt regulators	5743
MA	8562A-68	Diodes w/higher breakdown voltage improves focus reliability	5953
IO	8562A-69	YTF adjustment procedure	5938
MR	8563A-20C	Recommended replacement of 5-volt regulators	5744
IO	8563A-21	Incorrect manual procedure cannot measure resol B/W accuracy	5716
MA	8563A-22	Diodes w/higher breakdown voltage improves focus reliability	5954
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MA	8563E-07	Diodes with higher breakdown voltage improves focus reliability	5975
MR	8563E-08	5-volt regulator reliability improvement on A6 pc board	5925
IO	8566B-10B	Option 462 6 dB resolution bandwidths	5955
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MA	8568B-08A	RF attenuator with calibration ROM replacement	5691
TATT	8568B-10B	Option 462 6 dB resolution bandwidths	5956

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IO	8593E-01		
10	8593E-01 8593E-03	Additional equipment required during Option 012 calibration	5763 5988
0	8594E-01	List of specific test equipment reqd for Opt 151, 163 calib Additional equipment required during Option 012 calibration	5764
0	8594E-01 8594E-03	List of specific test equipment reqd for Opt 151, 163 calib	5989
0	8595E-01	Additional equipment required during Option 012 calibration	5765
10	8595E-01	List of specific test equipment required for Opt 151, 163 calib	5990
IO	8596E-01	Additional equipment required during Option 012 calibration	5766
10	8596E-03	List of specific test equipment required for Opt 151, 163 calib	5991
MA	8643A-01	RPP Module modification reduces noise floor of RF output	5721
IO	8643A-02	Jitter is normal for internal modulation source	5722
IO	8643A-03	Cable replacement and identification	5767
MA	8644A-01	RPP Module modification reduces noise floor of RF output	5723
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MR	8664A-03	Recommended replacement Reverse Power Protection assembly	
IO	8664A-04	Cable replacement and identification	5771
IO	8665A-03	Jitter is normal for internal modulation source	5730
MR	8665A-04	Recommended replacement Reverse Power Protection assembly	
IO	8665A-05	Cable replacement and identification	5772
IO	8665B-02	Jitter is normal for internal modulation source	5731
IO	8665B-03	Cable replacement and identification	5773
IO	8683A-03	Field support kit and assembly obsolescence	5700
IO	8683B-04	Field support kit and assembly obsolescence	5701
Ю	8683D-04	Field support kit and assembly obsolescence	5702
IO	8684A-05	Field support kit and assembly obsolescence	5703
ΙΟ	8684B-07	Field support kit and assembly obsolescence	5704
IO	8684D-05	Field support kit and assembly obsolescence	5705
MR	8711A-02	Cable replacement corrects display instability problem	5717
MR	8711A-03	Incorrect part in service kit/incorrect procedure in manual	5718
MR	8751A-17	Modification fixes unexpected spurious problem	5736
MR	8751A-22	Mod prevents hang ups or unexpected resets	5737
IO	8751A-24	New key cap for power line switch	5918
IO	8920A-07	Instructions for replacing the motherboard	5699
MR	8920A-08	Incorrect RF diagnostics results (Option 007)	5774
MR	8920D-01	Early units require FW upgrade for use with HP 11807A Opt 00	
MR	8920DTS-01	Early instuments require hardware and firmware upgrades	5959
MR	8921A-01	H/W and F/W upgrade required for 83201A compatibility	5749
MR	8921D-01	Early units require FW upgrade for use with HP 11807A Opt 00	
ΙΟ	8990A-01	Save A1 control board assembly top and bottom shields	5939
IO	8991A-01	Save A1 control board assembly top and bottom shields	5940
ΙΟ	8991A-02	Part number correction for the A1 control board assembly	5941
Ю	8992A-01	Save A1 control board assembly top and bottom shields	5942
MA	E1222M-09	Upgrade address space for error map to 1 Mbyte	5760
MR	E1300A-02	New time-delay fuse corrects intermittent fuse failure	5756
MR	E1301A-03	New time-delay fuse corrects intermittent fuse failure	5757
SA	E1401A-02-S	Recommended modification to prevent possible shock hazard	5758
MR	E1446A-01	New fuse prevents output from sticking at +24 or -24Vdc rail	5759
MR	E1672A-01	Mod reduces Trig output levels when loaded with 50 ohms	5936

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ю	E2500B-08	Changes to performance test software for pulse on/off tests	5752
IO	E2505A-01	New table provides correct ref designators during test 3xx	5753
IO	E2505A-02	Changes to performance test software for pulse on/off tests	5754
MR	E2550A-01	Mod corrects synchronization problems in parallel operation	5935
MR	E2550A-02	New firmware improves performance	5984
MR	E2755A-01	Mod improves reset and fixes crosstalk on F660 control board	5986
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MR	E3615A-01	New fuse eliminates intermittent blowing (Opt 0E3)	5972
MR	E3616A-01	New fuse eliminates intermittent blowing (Opt 0E3)	5973
MR	E3617A-01	New fuse eliminates intermittent blowing (Opt 0E3)	5974
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PS	E4095A/B-02-S	Inadequate ground may cause possible shock hazard	5964
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MR	J2213A-03	LED board mod allows greater range of brightness adjustment	
MR	J2219A-03	LED board mod allows greater range of brightness adjustment	
MR	11612A/B-01	Mod corrects open DC force path caused by incorrect wiring	5982
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MA	16099A-01		
MR	16339A-02	New flat-head mounting screws improve test fixture mounting	5920
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MR	34401A-03	Mod improves time stability of DC current ranges (10mA/100 r	,
IO	34401A-04	Explanation of indicated calibration failure of AC current	6002
MR	35280A-01	Repositioning int gnding lock washer elimis source sig probs	5999
MR	35650A-01	CR1 on ps brd fails due to excessive tightening of heat sink	6000
IO	35650B-01	Shield reduces magnetic emissions when fan assy replaced	5980
MR	35650B-02	Mod for use with 35659A Opt AMV or HO1	5987
MR	35652A/B-01	Mod improves reliability of microdot connector	5981
MR	35665A-02A	Mod corrects C1405A/B Keyboard failures	5922
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MR	37743A-01	Mod corrects incorrectly loaded capacitor on transmitter brd	5698
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MR	66000A-02	New resistor values for ac line input prevents failure	5957
MA	70001A-17A	New reset programmable array logic (PAL) integrated circuit	5983
MA	70004A-13	New PAL circuit allows MODRST line on A4 to be bi-directio	
IO	70301A-03	New 20 dB attenuator has longer semi-rigid cable	5707
MA	70320A-01	RPP Module modification reduces noise floor of RF output	5732
IO	70320A-02	Jitter is normal for internal modulation source	5733
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IO	70322A-02	Jitter is normal for internal modulation source	5734
IO	70322A-03	Cable replacement and identification	5776
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MA	70820A-02	Firmware revision 1.1 increases trace capability	5750

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MR	70908	A-07	-bl-st	Mod reduces n	x 300 MHz	residual responses	Service all	5751
MR	85032	B-01		Corrections to s	pec errors	in O/S manual and customer letter		5926
IO	85620	A-04		Module hangup	is caused t	y improper programming		5746
O	85620	A-05		Downloadable 1	programs m	ay not be compat w/earlier module	S	5943
MR	85644	A-02		Mod eliminates	1 MHz osc	on output of tracking source		5927
MR	85645	A-02		Mod eliminates	1 MHz osc	on output of tracking source		5928
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	MR	Modifi	cation R	ecommended	SA	Safety		
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("Optical Spectrum Analyzer," continued from page 2)

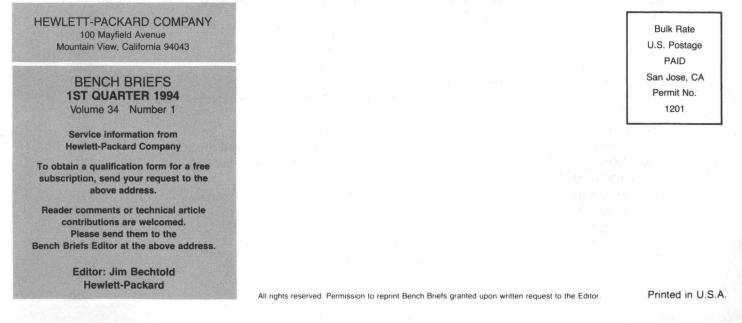
trace point reading. In all modes of operation, Hewlett-Packard optical spectrum analyzers zero the detector circuitry before each sweep.

Improved dynamic range is another benefit of sampling the stray light before each trace point. For measurements requiring the greatest dynamic range possible, some improvement can be obtained with the use of the chopper mode. While this mode does improve dynamic range, it is *not* required for the analyzers to meet their dynamic range specifications.

Figure 4 shows the improved dynamic range obtained by activating

the chopper mode.

This concludes the series on optical spectrum analyzers. *Bench Briefs* wants to thank Richard Ogg, Carla McCarter, and Mike Levernier of the Hewlett-Packard Microwave Technology Division/Lightwave Operation for their contributions to this series.



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